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Citation: [AIP Advances](#) **6**, 095313 (2016); doi: 10.1063/1.4963298

View online: <http://dx.doi.org/10.1063/1.4963298>

View Table of Contents: <http://aip.scitation.org/toc/adv/6/9>

Published by the [American Institute of Physics](#)

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## Separate density and viscosity measurements of unknown liquid using quartz crystal microbalance

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(Received 19 June 2016; accepted 9 September 2016; published online 19 September 2016)

Aqueous liquids have a wide range of applications in many fields. Basic physical properties like the density and the viscosity have great impacts on the functionalities of a given ionic liquid. For the millions kinds of existing liquids, only a few have been systematically measured with the density and the viscosity using traditional methods. However, these methods are limited to measure the density and the viscosity of an ionic liquid simultaneously especially in processing micro sample volumes. To meet this challenge, we present a new theoretical model and a novel method to separate density and viscosity measurements with single quartz crystal microbalance (QCM) in this work. The agreement of experimental results and theoretical calculations shows that the QCM is capable to measure the density and the viscosity of ionic liquids. © 2016 Author(s). All article content, except where otherwise noted, is licensed under a Creative Commons Attribution (CC BY) license (<http://creativecommons.org/licenses/by/4.0/>). [<http://dx.doi.org/10.1063/1.4963298>]

The quartz crystal microbalance (QCM) is a piezoelectric quartz crystal disc sandwiched between two electrodes, and it works in the thickness-shear mode when a voltage is applied across the electrodes. QCM translates the mass change on its surface into frequency shift and this qualifies QCM as a mass-sensitive device.

When a rigid film coats on the surface of a QCM, there will be a linear relationship between frequency shift and mass change on its surface. The quantitative equation was first proposed by Sauerbrey in 1959<sup>1</sup> as

$$\Delta f = -2nf_0^2 \frac{\Delta m}{\sqrt{\rho_q \mu_q}}, \quad (1)$$

where  $f_0$  is the fundamental frequency of the quartz crystal,  $\rho_0$  is the quartz density,  $\mu_q$  is the quartz shear elastic constant,  $\Delta m$  is the mass change, and  $n$  is the number of overtones. However, the Sauerbrey's equation can only be used for thin films rigidly attached to QCM surface in gas phase.

In fact, QCM is also a powerful device in a variety of technological applications and a versatile tool in a number of research fields. It is widely used to detect a variety of nanoscale target analytes in liquid environment, due to the advantages such as its simple operation, real-time output, and label-free analysis.<sup>2-5</sup> The applications of QCM in liquids are attracting increasing attentions.<sup>6</sup> The mechanism is not fully understood but prime factors causing the frequency changes are the viscosity and density of the liquids.<sup>6,7</sup>

When QCM is in contact with a liquid, the relation in Eq. 1 breaks down and a more complex relation exists between contacting liquid and frequency shift, due to the coupling of the crystal motion vibration with the surrounding liquid. Kanazawa and Gordon calculated the frequency change when one side of a quartz resonator is in contact with a liquid<sup>8</sup> and revealed that the frequency response of the QCM depends on the product of the density and the viscosity of the liquid. However, in the

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Kanazawa theory, the density and the viscosity can not be measured separately and the mass effect of the liquid is omitted, these greatly limit the application of the Kanazawa theory in liquids.

Due to the viscous coupling of the liquid medium to the QCM surface, device mass sensitivity is preserved.<sup>9</sup> It is also demonstrated that QCM driven in the thickness-shear-wave mode produces longitudinal pressure waves.<sup>10</sup> Martin and Allen tried to measure the density and the viscosity of a liquid separately by using two quartz resonators, a smooth-surface QCM and a textured-surface QCM.<sup>11</sup> Based on the Martin's theory, Atsushi Itoh *et al.* combined the frequency shift of QCM with admittance analysis (QCM-A) to measure the density and the viscosity of a liquid separately by using a textured-surface resonator.<sup>12</sup> Although these approaches mentioned above tried to discriminate the density and the viscosity measurements of a liquid but failed to separate changes in surface mass from changes in liquid properties when only the resonant frequency is monitored, and further concluded that it is impossible to separate liquid density and viscosity measurements with single QCM based on the frequency shift of QCM.<sup>11,12</sup>

In this work, we present a novel theoretical model and a new method to separate density and viscosity measurements of liquids only using a single smooth surface QCM based on the frequency response analysis.

When QCM sensor works in air or vacuum, it is only impacted by the stress. When there's liquid on the surface of the sensor, the sensor will be impacted by both the stress and the liquid pressure. And the frequency shift of the QCM sensor will be a result of the combined effects of both the stress and pressure variations:

$$\Delta f = K_{Pf} \Delta P f_0 + K_{Tf} \Delta T f_0 \quad (2)$$

where  $K_{Pf}$  is the pressure-frequency sensitivity coefficient,  $K_{Tf}$  is the stress-frequency sensitivity coefficient,  $\Delta P$  is the pressure variation,  $\Delta T$  is the stress variation,  $f_0$  is the reference frequency. The stress change caused by the liquid properties is:

$$\Delta T = C_{Lf} \sqrt{\rho_L \eta_L}, \quad (3)$$

where  $C_{Lf}$  is a coefficient describing the frequency shift of the bulk acoustic wave resonator sensor induced by the liquid property,  $\rho_L$  is the liquid density,  $\eta_L$  is the liquid viscosity.

The pressure change induced by the added liquid on upper surface of QCM sensor can be given as:

$$\Delta P = \rho_L C_{Pf} V_L, \quad (4)$$

where  $C_{Pf}$  is the pressure frequency coefficient,  $V_L$  is the liquid volume loaded onto the sensor surface.

Obviously, once a liquid sample is loaded on QCM, the stress variation of the QCM sensor induced by the liquid viscosity and density is determined and the frequency shift induced by the liquid property is also determined,  $K_{Tf} \Delta T f_0$  will be a constant. It's the frequency variations resulted from different volumes of liquid that can approach the density of it and then the viscosity. Theoretical expressions of the density  $\rho_L$  and the viscosity  $\eta_L$  are:

$$\rho_L = \frac{nD(\Delta f_2 - \Delta f_1)}{K_{Pf} C_{Pf} \Delta V f_0^2} \quad (5)$$

and

$$\eta_L = \frac{K_{Pf} C_{Pf}}{(\Delta f_2 - \Delta f_1) f_0 \Delta V} \left[ \frac{\Delta f_1 \Delta V - V_{L1}(\Delta f_2 - \Delta f_1)}{K_{Tf} C_{Lf}} \right]^2 \quad (6)$$

respectively, where  $n$  is the overtone number,  $D$  is the diameter of QCM electrodes,  $\Delta V$  is the volume increment after the second liquid addition,  $\Delta f_1$  is the frequency shift after the first liquid addition,  $\Delta f_2$  is the frequency shift after the second liquid addition,  $f_0$  is the reference frequency,  $K_{Pf}$  is the pressure-frequency sensitivity coefficient and  $K_{Pf} = f_0 K_f / nD$ ,  $K_f$  is pressure-frequency coefficient and  $K_f = -23.3 \times 10^{-15} (msN^{-1})$ ,  $K_{Tf} = -2.75 \times 10^{-11} (m^2/N)$  is the stress-frequency sensitivity coefficient,<sup>13,14</sup>  $C_{Pf}$  is the pressure-frequency coefficient in liquid phase,  $C_{Lf}$  is the liquid phase stress-frequency coefficient in liquid phase,  $V_{L1}$  is the first volume of liquid added to the QCM.

Fig. 1 shows the schematic of the experimental setup consisting of a micro-pipet (Model EpT.I.P.S. @10 $\mu$ L, Eppendorf), a Universal Counter (Model 53132A, Agilent), and a QCM sensor

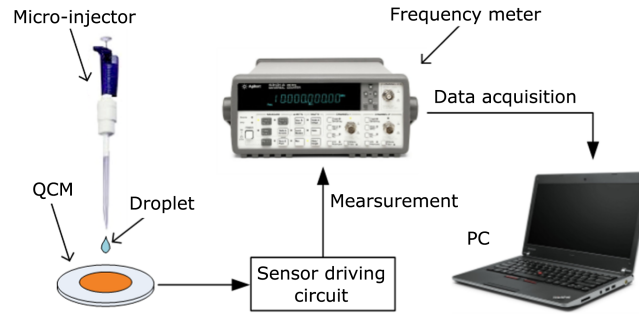


FIG. 1. Schematic of measuring liquid properties with QCM.

driving circuit. In this study, an AT-cut QCM with 3<sup>rd</sup> overtone at 10MHz and conventional thermally evaporated gold electrodes are used (Tongfang Guoxin Electronics Co., Ltd.). The diameter of the gold electrode is 5mm.

Pure water is chosen as the reference sample and aqueous solutions with NaCl concentrations of 10%, 20%, and 30% are prepared as target samples. NaCl is obtained from Sigma Aldrich and diluted with DI water. Measurements are performed at room of 25°C and frequency shifts are recorded. Table I shows the frequency shifts for NaCl solution with different concentrations, where  $V$  is the volume of the liquid added to the electrode.

During the experiments, if the volume of the liquid is less than 4μL, the electrode of the QCM cannot be covered completely. If the electrode of the QCM is not covered completely, the frequency shift varies nonlinearly as the liquid volume changes. Only when the liquid covers the electrode completely, there exists a linear relationship between the frequency shift and the added liquids in some volume ranges. Fig. 2 shows the fitting plots of the frequency shifts of QCM for pure water, NaCl, HCl and KCl solutions with different volumes. It can be concluded that for a given liquid, it features determined attributes (density and viscosity), causing constant QCM frequency shift. When the QCM electrode is covered incompletely, the liquid attributes and the liquid mass effect work together to make the frequency vary nonlinearly. After the electrode is covered completely, only the liquid mass effect works, which makes a linear frequency variation.

In this work, take the pure water as a reference sample, and the parameters  $\rho_W = 1.0 \times 10^3 \text{ kg/m}^3$  and  $\eta_W = 8.949 \times 10^{-4} \text{ Pa} \cdot \text{s}$ , where  $\rho_W$  and  $\eta_W$  denote the density and the viscosity of the pure water, respectively. We first determine coefficients of  $C_{Pf} = 7.3903 \times 10^4 \text{ m/s}^2$  and  $C_{Lf} = -1.2877 \times 10^6 \text{ m}^3/\text{s}^2$ . And then, let  $\Delta f_1$  be the frequency shift at  $V = 4\mu\text{L}$ , and  $\Delta f_2$  is frequency shift at  $V = 6\mu\text{L}$ , 8μL and 10μL, respectively. With Eq. 5 and Eq. 6, the density and viscosity of the NaCl, HCl and KCl solutions with different concentrations are calculated and given in Table II. To test our analysis module, we use Cannon-Fenske viscometer(Aldrich) in a thermostated bath tested the viscosity of the three NaCl solution samples of different density respectively. For the other two liquids, we compared the results with the data in literatures.<sup>15–17</sup> Comparing our experiment results, we find there are errors between our results by using QCM sensor and results in literatures and the results by using Cannon-Fenske

TABLE I. Frequency shifts in different volumes of liquid samples.

Volume	Pure-water $\Delta f$ (Hz)	NaCl(wt%)/ $\Delta f$ (Hz)			HCl(wt%)/ $\Delta f$ (Hz)			KCl(wt%)/ $\Delta f$ (Hz)		
		10%	20%	30%	10%	20%	30%	10%	20%	30%
0μL	0	0	0	0	0	0	0	0	0	0
2μL	-165	-189	-263	-285	-193	-223	-267	-147	-186	-271
4μL	-280	-308	-351	-388	-300	-330	-366	-289	-302	-315
6μL	-303	-330	-378	-414	-325	-352	-391	-313	-331	-345
8μL	-325	-355	-409	-441	-345	-382	-419	-341	-356	-370
10μL	-346	-388	-422	-479	-369	-404	-443	-362	-372	-393

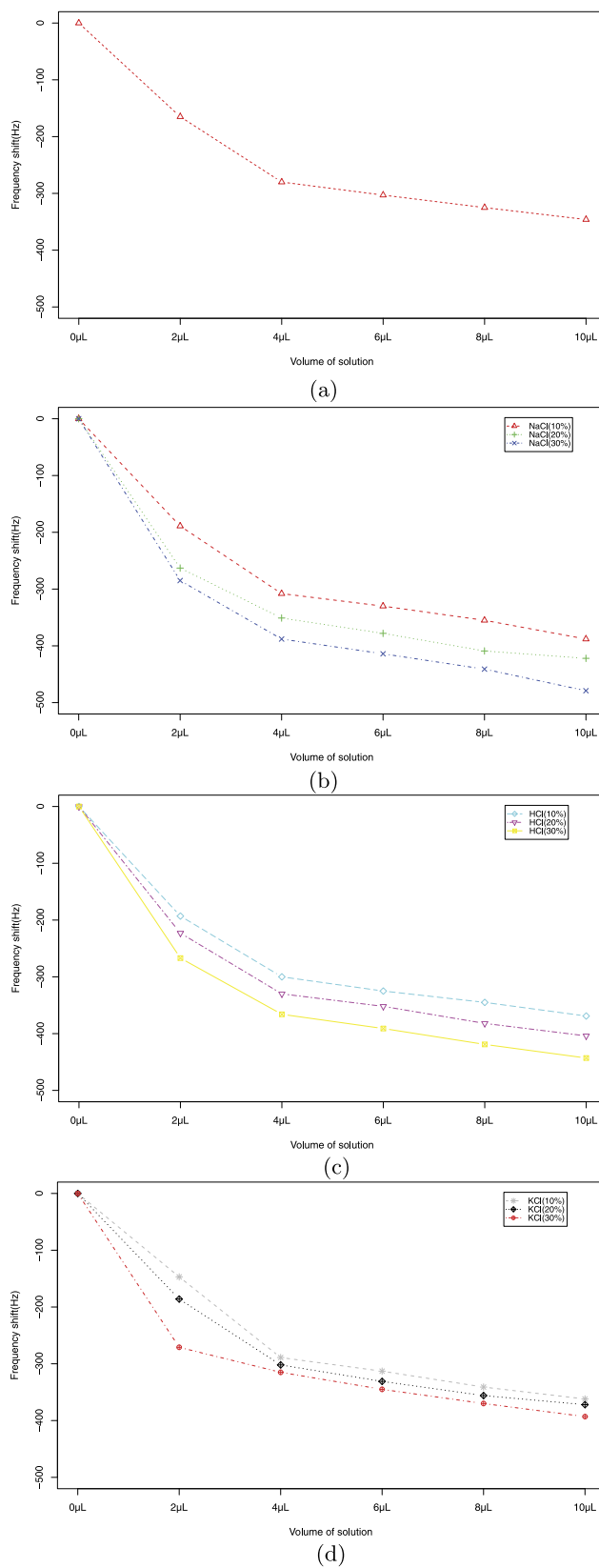


FIG. 2. Frequency shifts measured for pure water, NaCl, HCl and KCl samples.

TABLE II. Density and viscosity of NaCl, HCl and KCl solutions at 25°C.

(a) NaCl				
NaCl(wt%)	Ref. Value Density( $g/cm^3$ )	QCM Measured Avg. Density ( $g/cm^3$ )	Cannon-Fenske Viscometer Measured Dynamic Viscosity ( $mPa \cdot s$ )	QCM Measured Avg. Viscosity ( $mPa \cdot s$ )
10%	1.0680 <sup>15</sup>	1.0691	1.0426	1.0992
20%	1.1450 <sup>15</sup>	1.1802	1.2602	1.3051
30%	1.1729 <sup>16</sup>	1.2292	1.5549	1.5563
(b) HCl				
HCl(wt%)	Ref. Value Density( $g/cm^3$ )	QCM Measured Avg. Density ( $g/cm^3$ )	Ref. Value <sup>17</sup> Dynamic Viscosity ( $mPa \cdot s$ )	QCM Measured Avg. Viscosity ( $mPa \cdot s$ )
10%	1.0500	1.0444	1.0524	1.0607
20%	1.1000	1.0765	1.2243	1.0719
30%	1.1500	1.1432	1.5055	1.4829
(c) KCl				
KCl(wt%)	Ref. Value <sup>15</sup> Density( $g/cm^3$ )	QCM Measured Avg. Density ( $g/cm^3$ )	Ref. Value <sup>15</sup> Dynamic Viscosity ( $mPa \cdot s$ )	QCM Measured Avg. Viscosity ( $mPa \cdot s$ )
10%	1.0640	1.1012	0.8911	0.9059
20%	1.1080	1.1753	0.9080	0.9295
30%	1.1690	1.2370	0.9378	0.9520

Viscometer. The error depends on the following aspects: (1) The cleanness of the QCM sensor surface. The cleaner QCM surface is, the smaller the error is. Before each measurement, the sensor must be cleaned and dried completely. (2) The work state of the driving circuit of QCM sensor. If the work state of the driving circuit is unstable, the frequency of the QCM sensor will jump in experiment and the error will get bigger. So it's important to maintain a stable work state of the driving circuit. (3) Environment. Putting the sensor and the driving circuit in a thermostatic chamber can lower the error. (4) The stability and accuracy of reference source of the frequency meter. A reference source with high stability and high accuracy to the frequency meter can help to lower the error. Testing accuracy is influenced by the parameters of QCM, accuracy of liquid concentration, environment temperature, and reference clock source in Counter, etc. Of course, the working state of the QCM driving circuit is a very important factor as well.

In conclusion, this paper presents a new model and a novel method to separate density and viscosity measurements of liquids based on the frequency response analysis of QCM, and the experimental results demonstrate its feasibility. The authors will focus on improving the accuracy in the future work.

This work was financially supported by the Fundamental Research Funds for the Central Universities (NO.ZYGX2014J067, ZYGX2015J077) and the Innovation Program from Ministry of Science and Technology (NO. 2013IM020400), and the authors wish to thank Zi-Yang Jia for assistance.

<sup>1</sup> G. Sauerbrey, *Zeitschrift für Physik* **155**, 206 (1959).

<sup>2</sup> E. J. Cho, L. Yang, M. Levy, and A. D. Ellington, *Journal of the American Chemical Society* **127**, 2022 (2005).

<sup>3</sup> M. Hieda, R. Garcia, M. Dixon, T. Daniel, D. Allara, and M. H. W. Chan, *Applied Physics Letters* **84**, 628 (2004).

<sup>4</sup> P. Wang, J. Su, W. Dai, G. Cernigliaro, and H. Sun, *Applied Physics Letters* **104**, 043504 (2014).

<sup>5</sup> J. Lee, J. Jang, D. Akin, C. A. Savran, and R. Bashir, *Applied Physics Letters* **93**, 013901 (2008).

<sup>6</sup> C. Barnes, *Sensors and Actuators A: Physical* **30**, 197 (1992).

<sup>7</sup> D. M. Soares, W. Kautek, C. Fruböse, and K. Doblhofer, *Berichte der Bunsengesellschaft für physikalische Chemie* **98**, 219 (1994).

<sup>8</sup> K. K. Kanazawa and J. G. G. II, *Analytical Chemistry* **57**, 1770 (1985).

- <sup>9</sup> M. D. Ward, D. A. Buttry *et al.*, *Science* **249**, 1000 (1990).
- <sup>10</sup> S. M. Reddy, J. P. Jones, and T. J. Lewis, *Journal of Applied Physics* **83**, 2524 (1998).
- <sup>11</sup> S. J. Martin, K. Wessendorf, C. Gebert, G. Frye, R. Cernosek, L. Casaus, and M. Mitchell, “Measuring liquid properties with smooth-and textured-surface resonators,” Tech. Rep. (Sandia National Labs., Albuquerque, NM (United States), 1993).
- <sup>12</sup> A. Itoh and M. Ichihashi, *Measurement Science and Technology* **22**, 015402 (2011).
- <sup>13</sup> J. M. Ratajski, in *20th Annual Symposium on Frequency Control. 1966* (IEEE, 1966), pp. 33–49.
- <sup>14</sup> E. EerNisse, *Journal of Applied Physics* **43**, 1330 (1972).
- <sup>15</sup> F. A. Gonçalves and J. Kestin, *Berichte der Bunsengesellschaft für physikalische Chemie* **81**, 1156 (1977).
- <sup>16</sup> A.-M. R. L. G. Andrei Ionuț Simion and C.-G. Grigoraș, *Journal of Agroalimentary Processes and Technologies* **21**, 41–52 (2015).
- <sup>17</sup> E. Nishikata, T. Ishii, and T. Ohta, *Journal of Chemical and Engineering Data* **26**, 254 (1981).